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**AN ELASTOMER ACTUATOR AND**  
**A METHOD OF MAKING AN ACTUATOR**

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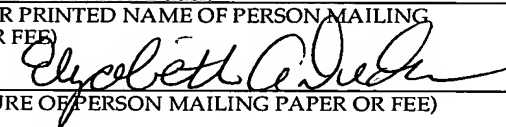
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**AN ELASTOMER ACTUATOR AND A METHOD OF MAKING AN ACTUATOR****INTRODUCTION**

The present invention relates to an actuator, e.g. for use in robotic applications. The actuator could be made from a sheet comprising a plate shaped element with an elastomeric body confined between electrodes. The electrodes are arranged with respect to the elastomeric body to deform the body upon application of an electrical field to the electrodes. The plate shaped element is rolled into a cylindrical structure capable of expanding and contracting, respectively, upon application of an electrical potential to the electrodes.

**10 BACKGROUND OF THE INVENTION**

Elastomer actuators with electrodes for deflecting an elastomeric material are known to facilitate large deformation in a relatively low electric field, e.g. when compared with alternative dielectric materials, e.g. piezoelectric materials including ceramics. The principle of operation is that an electrical potential between two electrodes generates an electrical field leading to a force of attraction or repulsion. As a result, the distance between the electrodes changes which leads to compression or tension of the elastomeric material which is thereby deformed. Due to the similarity between the principle of operation and the functioning of a muscle, an elastomer actuator is sometimes referred to as an Electrostrictive Polymer Artificial Muscle (EPAM).

Typically, elastomer actuators are made by applying a conductive electrode, e.g. a carbon containing paint or a thin layer of gold to both sides of a film made from an elastomeric material e.g. Silicone or Polyurethane. The film is typically made in a moulding process. Laminated actuators are known, e.g. from US 5,977,685, disclosing layers of a polyurethane elastomer with electrodes on each side, laminated together to form a deformable sheet. Each layer has slit gaps formed in a horizontal direction, whereby the layer maintains the volume during a shrinkage displacement.

E.g. in order to save space, elastomer sheets can be rolled up to form cylindrical actuators to replace more traditional linear actuators in multiple small-scale systems, e.g. in robotic applications forming legs or grippers of a robotic wrist etc. In the heretofore seen rolled actuators, the film is rolled into a tubular portion fitted with mechanical connectors at axially opposite ends. Upon application of an electrical field to the electrodes, the sheet contracts or expands axially during deformation of the elastomeric material. It has, however, been found, that the

rolled configuration of the elastomer film to a certain extent limits the ability of the film to deform and thus reduces the performance. In particular when the cylindrical actuator is designed for longitudinal expansion and contraction, it is necessary that the longitudinal change in length is compensated by a radial constriction of the cylindrical actuator, and since a cylindrical shape of a body implies stiffness towards radial constriction, the cylindrical shape limits the extent of longitudinal expansion and contraction. Until now, a maximum stroke in the order of 5-7 percent of the length of the rolled cylindrical actuator is typically accepted as the limit of the technology.

## 10 DESCRIPTION OF THE INVENTION

In accordance with the present invention, provision is made for an actuator made from an elastomer film and which facilitates an improved performance. Accordingly, the present invention in a first aspect provides an actuator comprising a tubular portion extending in a longitudinal direction, the tubular portion comprising a body of an elastomeric material arranged between two electrodes, wherein any line of symmetry extending between two opposite points on a periphery in a cross-section perpendicular to the longitudinal direction has a length which is different from any other such line of symmetry.

In other words there may be provided an actuator with a cross-section having no lines of symmetry, one single line of symmetry or a plurality of lines of symmetry all being of different lengths.

As an example, the shape may be non-circular or non-quadrangular. As an example, the actuator may, in that cross-sectional view, expose two axes of symmetry having different length. As an example, the actuator may, in the above mentioned cross-sectional view, have an oval shape, it may have the shape of an egg or it may be rectangular.

When an electrical potential is applied over the electrodes, the electrical force of attraction or repulsion forces the electrodes toward or away from each other whereby the elastomeric material is deformed. Due to the specific shape, it is achieved that the proportions of the tubular portion in directions perpendicular to the longitudinal direction are free to change during longitudinal expansion and contraction and therefore, the ability of the actuator to expand and constrict in the direction perpendicular to the longitudinal direction is improved when compared with actuators e.g. having a circular or a quadrangular cross-sectional shape, i.e. actuators exposing multiple axes of symmetry having equal length. Accordingly, a larger longitudinal expansion and contraction can be achieved.

Preferably, and in order to facilitate an easy manufacturing, the tubular portion may be formed by rolling up a sheet comprising at least two elements each comprising a body of an elastomeric material and an electrode attached to a first surface thereof, wherein deformation of the body and/or the electrode is restricted in a first direction and supported in a another, second, direction. The second direction may preferably be parallel to the longitudinal direction. Due to the restriction and supporting of deformation, respectively, it is achieved that the body deforms only, or at least primarily, in one direction, i.e. the deformation occurs in the longitudinal direction while the restriction of deformation is circumferentially around the tubular portion, leading to a conservation of the perimeter of the tubular portion.

The body may be a dielectric body and as will be described in further details, it may preferably have a plurality of corrugation on at least one surface and it may preferably have anisotropic properties. The two elements are stacked so that a surface of one of the elements is in contact with a surface of another element.

The restriction and supporting of the deformation in the two directions may be achieved e.g. by forming corrugations in the electrodes and in the elastomeric bodies. The corrugations could extend mutually parallel in the first direction and thus support deformation in the second direction being perpendicular to the first direction. The corrugations could be formed during manufacturing of the elastomeric body in a moulding process. By vaporising a conductive material, e.g. gold, silver, copper, aluminium, or any similar conductive metal onto the body in a subsequent process, a very thin electrode may be formed onto the corrugations of the body. The electrode will effectively prevent deformation in the direction of the corrugations.

Preferably, supply paths in the form of conductive terminals are connected to each of the at least two elements to apply different electrical potentials to the corresponding electrodes. In order to make connection of a power source easier, the sheet may comprise:

- an element of a first type comprising a conductive terminal of a first type being in electrical contact with the electrode of the element
- an element of a second type comprising a conductive terminal of a second type being in electrical contact with the electrode of the element,

wherein the conductive terminal of the first type is electrically isolated from the conductive terminal of the second type when the elements are stacked to form a sheet of alternating elements of the first and second type. As an example, the terminals may be exposed on the surface of the elastomer bodies on alternating different locations, e.g. so that every second element has a terminal at a rightmost end of the element and every other second element has a terminal at a leftmost end

of the element, when the elements are stacked to form a sheet. In the sheet, the elastomer material of the bodies forms isolation between the terminals of adjacent elements.

5 Preferably the rolled structure consists of alternately one element of the first type and one element of the second type. The element of the first type is connected to a first supply path and the element of the second type is connected to a second supply path. Hereby is achieved that a single working layer in the laminated structure consists of one electrode on one first element, one body of one second element and one electrode on one second element. Another layer in the laminated  
10 structure consists of one electrode on one second element, one body of one first element and one electrode on one first element.

The element of the first type may further comprise a conductive terminal of a second type being electrically isolated from the electrode of the element. Correspondingly, the element of the second type may comprise a conductive  
15 terminal of a first type being electrically isolated from the electrode of the element. When the conductive terminals of the first type are in mutual electrical contact and the conductive terminals of the second type are in mutual electrical contact, e.g. when the elements are stacked, all terminals of the first type may be connected to one terminal of a power source at one connection point and all terminals of the  
20 second type may be connected to another terminal of the power source at another connection point. The terminals which are electrically isolated from the electrode of the element serve to bridge the electrical potential difference across the element between two adjacent elements.

In order further to facilitate application of the power source, the conductive  
25 terminals of the first and/or the second type may cover peripheral rim portions of the bodies of the elastomeric material, e.g. so that the terminals of the first type cover the rim portion at one location and the terminals of the second type cover the rim portion at another location, when the elements are stacked to form a sheet of alternating elements of the first and second type. Conductive wires attached to the  
30 terminals along the rim portions may thus connect the electrodes with a power source.

In a specific embodiment of the invention, the rolled structure is formed by rolling the elements around an elastomer core. In order to reduce the impact of the core on the compliance of the rolled actuator, the elastomer core may be softer than the  
35 elastomer of the bodies of the actuator.

In a specific drum shaped embodiment of the invention the rolled structure exposes a cavity limited by the tubular portion, i.e. limited by the rolled structure, and two closure parts fastened at axially opposite ends of the tubular portion. The closure

parts may have the shape of axle journals, e.g. comprising fastening means for attaching the actuator to an application, e.g. a robotic handgrip. Hereby is achieved that the rolled structure exposes a cylindrical cross-section where the core of the structure is a passive cavity. The core of an elastomer material could be made by  
5 filling the cavity with an elastomer material, e.g. in a liquid state. Subsequently, the liquid core is hardened, e.g. while the rolled structure is stretched axially. Hereby is achieved that the body of the structure exposes compressive stress while the core is filled and hardened. When the structure afterwards is released axially, the  
10 compressive stress of the body will induce tensile stress in the core, and the force balance will result in a stable self-supporting structure, when the actuator is in a released inactivated position.

In a second aspect, the present invention relates to a method of making a rolled elastomer actuator, said method comprising the steps of:

- 15 – forming a sheet from layers of elements, each comprising a body of an elastomer material and an electrode in contact with a surface of the body,
- rolling up the sheet to form a hollow tubular portion with a shape wherein any line of symmetry extending between two opposite points on a periphery in a cross-section perpendicular to the longitudinal direction has a length which is different from any other such line of symmetry, e.g. into an oval or  
20 rectangular shape.

The method according to the second aspect may be extended to cover steps for making an actuator according to any of the features of the first aspect of the invention, and in particular, the tubular portion may be filled with a liquid elastomer material which is subsequently hardened to form an elastomer core for the tubular  
25 portion.

#### DETAILED DESCRIPTION OF THE INVENTION

In the following, a preferred embodiment of the invention will be described in further details with reference to the drawing in which:

Fig. 1 shows a first plate shaped element of the actuator,

30 Fig. 2 shows a second plate shaped element of the actuator,

Fig. 3 shows a laminated actuator,

Fig. 4 shows the laminated actuator in a top view,

Fig. 5 is a cross-sectional view in radial direction of a rolled actuator,

Fig. 6 shows a cross-sectional view in longitudinal direction of a rolled actuator,

Fig. 7 shows the assembling sequence for the assembling of two elements into one sheet, and

Figs 8a-8d show filling of a cavity of the rolled structure with a liquid elastomer.

Fig. 1 shows a plate shaped element 1 for a laminated stack forming a sheet for an actuator. The element consists of a body 2 of an elastomeric material. The body has a corrugated profile on one of its two surfaces, and an electrode 3 deposited on a large part of the corrugated surface. The electrode is deposited onto the surface of the body in a thickness of a few hundreds of Angstroms e.g. by vapour deposition of conductive particles onto the surface. The electrode could be made from gold, silver, and copper or from any conductive material.

The corrugations of the body 2 are not shown in Fig. 1 but they should be understood to be corrugations, e.g. with a quasi-sinusoidal or a curved cross-sectional shape e.g. with a corrugation height from the top of a corrugation to the bottom of the corrugation in the order of  $1/3$ - $1/5$  of the total thickness of the elastomer body. As an example, the corrugation height of a body having a total thickness of  $20\text{ }\mu\text{m}$  could be in the size of  $5\text{ }\mu\text{m}$ . With respect to the orientation of the body 2 and electrode 3 of Fig. 1, the corrugations extend in a horizontal direction, i.e. in the direction indicated by the arrow, cf. numeral 8. The body 2 including the corrugations is made e.g. in a moulding process from a silicone or rubber material or from any elastomer.

When the electrode is deposited onto the corrugated surface of the body 2, e.g. by vaporisation, the electrode will form a thin metal layer with corrugations corresponding to the corrugations of the body. As a result, the element, and thus a sheet made from a plurality of elements becomes more flexible in a direction perpendicular to the corrugations, i.e. in a vertical direction indicated by arrows 4 in Fig. 1 than in directions non-perpendicular to the corrugations, e.g. in the horizontal direction in Fig. 1. This structure gives the element and thus a sheet made from elements anisotropic properties. Due to the anisotropic properties and the fact that the volume of the element is conserved during deformation, it is achieved that a compression or expansion of the thickness of the element will be transformed mainly into deformation in the direction perpendicular to the corrugations, i.e. in the vertical direction of Fig. 1.

Two conductive terminals 5 and 6 are shown on top of the electrode 3. One terminal 5 constitutes an electrical path to the electrode 3. The other terminal 6 is made from an electrically conductive material but it is, however, not connected to the electrode 3. By facilitating connection of an electrical source, the terminals 5, 6 serve for connection of a power source to establish an electrical potential difference between electrodes of adjacent elements, when the elements are stacked to form a laminated structure.

Fig. 2 shows a plate shaped element 7 similar to that of Fig. 1, but wherein the supply path 6 constitutes a conductive terminal connected to the electrode 3, and wherein the supply path 5 is not connected to the electrode 3. This gives two different plate shaped elements. In the following, the element with numeral 1 is to be referred to as a plate shaped element of a first type and the element with numeral 7 is referred to as a plate shaped element of a second type.

Fig. 3 shows a side view of an actuator 9 in the form of a structure laminated from elements comprising bodies made from an elastomeric material 2 and an electrode 3. In order to visualise the structure more clearly, the thicknesses of the bodies and the electrodes are shown without considering right proportions. In reality, the electrodes may be vaporised on the elastomeric body 2, whereby the total thickness of a single element 1, 7 is limited to around 15-30  $\mu\text{m}$ , of which the electrode has a thickness of a few hundreds of Angstroms. Accordingly, the laminated actuator 9 forms a flat sheet structure. In the laminated structure of the actuator 9 elements of the first type 1 is arranged adjacent and alternating elements of the second type 7 thereby forming two conductive connection paths extending along the peripheral rim portion of the actuator for connecting an electrical source for establishing an electrical potential difference between electrodes of adjacent elements in the actuator.

The cross section a-a of Fig. 4 indicates the view shown in Fig. 1, and the cross section b-b indicates the view shown in Fig. 2. The two terminals 5 and 6 are connected to an electrical high voltage source via conductive wires 11 attached to the terminals along the rim portions of the terminals. This connection gives the electrode of elements 1 and 7 different potentials, and the induced electrical field will pull the electrodes towards each other. This will result in a shrinkage displacement of each of the bodies 2, indicated by arrows 10 on Fig. 4, whereby the vertical displacement of the actuator will occur, indicated by arrows 4 in Figs. 1, 2 and 3.

The force developed by the actuator increases with the number of elements in the laminated structure. A sealing sheet 12, consisting of a body of the same elastomer as the first and second element, is closing the laminated structure, whereby the electrode of the last element is sealed and electrically insulated from the



surroundings. A sealing sheet 12 is arranged in contact with an electrode of an adjacent element.

The actuator 9 in Figs. 3 and 4 is plate shaped and the degree of force which the actuator can exert depends on the number of elements included in the laminated sheet and on the cross-sectional area of each element. Fig. 5 shows a structure for an actuator 13, wherein the two plate-shaped elements 1, 7 are laminated together to form a sheet which is subsequently rolled. In this structure where only two elements are laminated and rolled, the degree of force depends mainly on the number of windings. In Fig. 5 the actuator 13 comprises 3 windings of a sheet made from an element of a first type and an element of a second type. Due to the rolling, the actuator forms a cylindrical shape.

Due to the corrugation of the elements including the electrodes, the actuator becomes very compliant to deflect in one direction, and less compliant in other directions. By rolling the elements into a roll having a longitudinal axis perpendicular to the corrugations, the actuator becomes compliant to extend and shorten in the longitudinal direction, whereas it is stiff in the direction of the corrugations. Due to volume conservation of the elastomeric polymeric bodies in the elements forming the sheet, radial constriction and swelling of the actuator is necessary during longitudinal extending and shortening. Since changes to the cross-sectional area is impossible without changing the perimeter of a circular rolled actuator, a circular cross-sectional shape will exert more resistance towards the radial constriction. However, in an oval, e.g. an elliptic or rectangular cross-sectional shape as shown in Fig. 5, different ratios between the extent in the "a" and "b" directions will expose different areas for the same perimeter and thus facilitate radial constriction and thus longitudinal extending and shortening of the rolled actuator.

In further details, the following applies for a rolled sheet with a circular cross sectional shape:

$$\text{Perimeter} = 2 * \pi * r$$

$$\text{Area} = \pi * r^2$$

$$\text{Volume} = \text{Area} * \text{length}$$

wherein r denotes the radial dimension of the roll. Since the length is changed, and the Volume is fixed, the area has to be changed. The area can only change as a result of changes to the radius which, in theory, is not possible and, in practise, very difficult due to the perimeter conservation. On the contrary, the following applies for a rolled sheet with an elliptical, i.e. a non-circular cross sectional shape:

$$Perimeter = 2 * \pi * \sqrt{\frac{a^2 + b^2}{2}}$$

$$Area = \pi * a * b$$

$$Volume = Area * length$$

- 5 wherein a and b represents the half the lengths of the two axes of symmetry in the ellipse. Accordingly, it is easier to extend and shorten the rolled actuator having an elliptical cross-sectional shape since it is possible to find different value sets of a and b where each set results in a constant perimeter value while the area changes.

Multiple geometries of non-circular cross-sectional shapes facilitate changes to the area without changing the perimeter of which one is shown in Fig. 5.

- 10 Fig. 6 shows a cross-sectional view of the actuator 13 parallel to the longitudinal direction. A cavity 15 is confined between the rolled structure 1, 7 and the two closure parts in the shape of axle journals 14. The axle journals have an outer cross sectional shape which corresponds to the inner cross sectional shape of the tubular portion.
- 15 The sheet made from the plate shaped elements 1 and 7 is rather soft. The actuator structure is therefore also rather soft, and, depending upon the specific material and thicknesses of the elements 1, 7 the actuator will be unable to support itself when it is not mounted in an application or fixture. In order to stabilise the actuator, and make handling easier, the cavity 15 is filled with a soft elastomer material, e.g.
- 20 through at least one of the holes 16. This filling of the cavity 15 occurs while the actuator is stretched axially, e.g. by means of a fixture. When the elastomer material inside the cavity 15 is hardened, it exposes a deformable elastomer body, of a softer nature than the elastomer bodies of the elements 1 and 7. When the axially stretched actuator is released, the two axle journals will be pulled together,
- 25 which will deform the material inside the cavity 15. Compressive and tensile stress balance in this mechanical structure will result in a self-supported rolled actuator.

- Fig. 7 shows an element of a first type 20 and an element of a second type 21. The element of the first type comprises a conductive terminal 22 of a first type and a conductive terminal 23 of a second type. The elements are stacked to form a sheet
- 30 24 comprising alternating elements of the first type 20 and elements of the second type 21, i.e. in which the conductive terminals are placed at opposite sides of the elastomeric body 25.

Figs. 8a-8d show the process of filling the cavity 30 with a liquid elastomer material. In Fig. 8a, the actuator is ready for the elastomer core to be filled into the cavity through the openings 31 formed in the axle journals. In Fig. 8b, the actuator is stretched axially prior to the filling. In Fig. 8c, the liquid elastomer core is filled into the cavity and In Fig. 8d, the core is cured, e.g. inside an oven symbolised by the line 32.